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**The applicability  
of Monin–Obukhov scaling  
for sloped cooled flows  
in the context of  
Boundary Layer parameterization**

**The low-level katabatic jet  
height versus  
Monin–Obukhov  
height**

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# Outline

Overview of ABL(PBL) parameterization :

- importance for describing ABL
- general approaches in modeling
- problems

SABL (VSABL)

- nature and modeling features
- Monin-Obukhov height ( $L$ ) and the low-level jet (LLJ) height

Conclusions

# Background & overview

stable boundary layers are still not well understood.

turbulence can be of different nature and properties than that generated over nearly-horizontal surfaces.

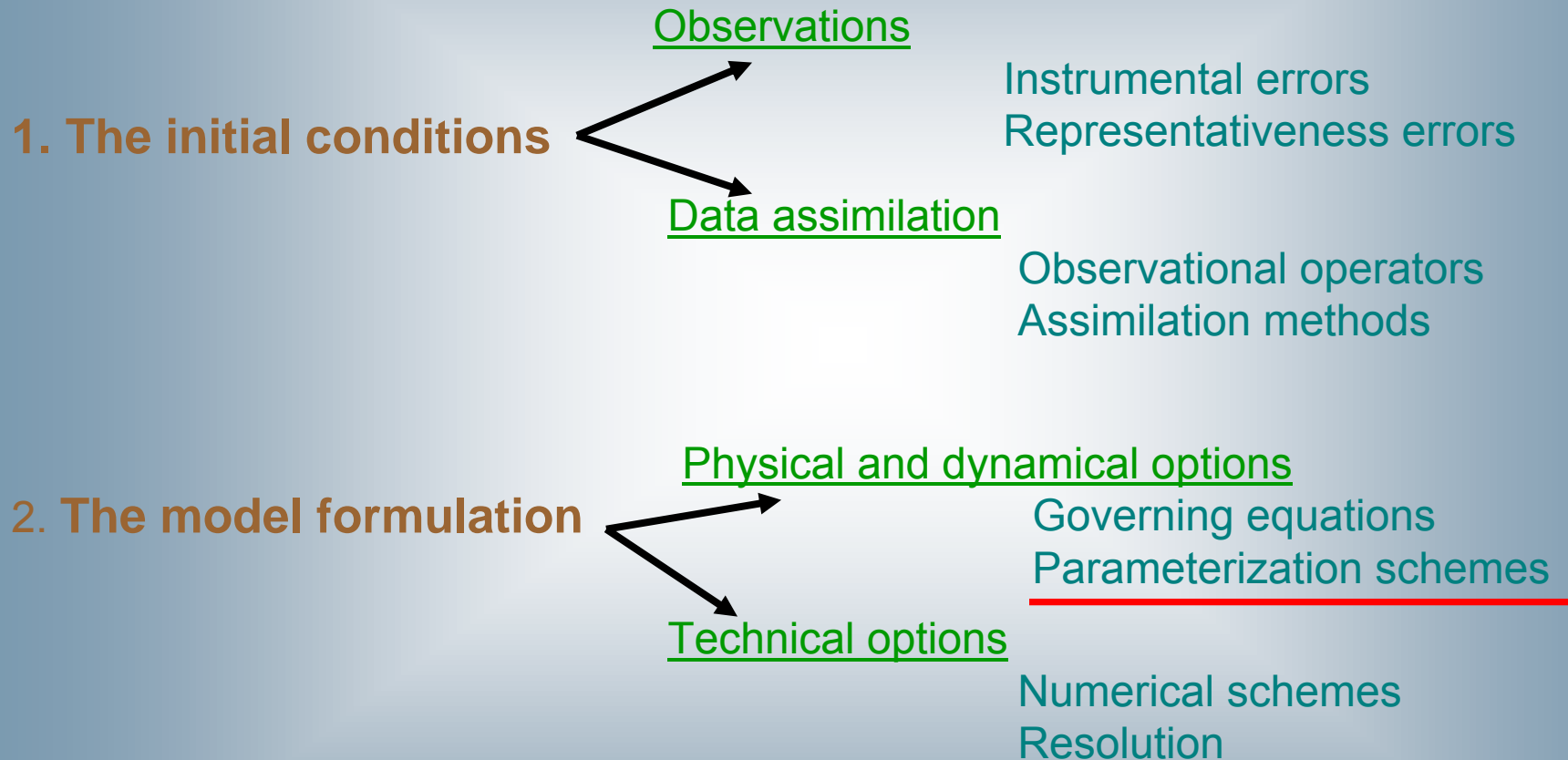
Monin-Obukhov length,  $L$ , for parameterizing near-surface turbulent fluxes is widely used in NWP etc., but still questionable for katabatic flows.

for estimating  $z_j$  used the Prandtl model (Prandtl, 1942; Defant, 1949).

Baklanov and Grisogono, 2007  
Banta, 2008  
Cuxart and Jiménez, 2007;  
Grisogono and Belušić, 2008  
Grisogono and Oerlemans, 2001;  
Jeričević and Grisogono, 2006  
Kim and Mahrt, 1992;  
King et al., 2001;  
Mahrt, 1998, 2007, 2008;  
Mauritsen et al., 2007;  
Steeneveld et al., 2007;  
Söderberg and Parmhed, 2006;  
Van der Avoird and Duynkerke, 1999;  
Zilitinkevich et al., 2008  
Zilitinkevich and Esau (2007)

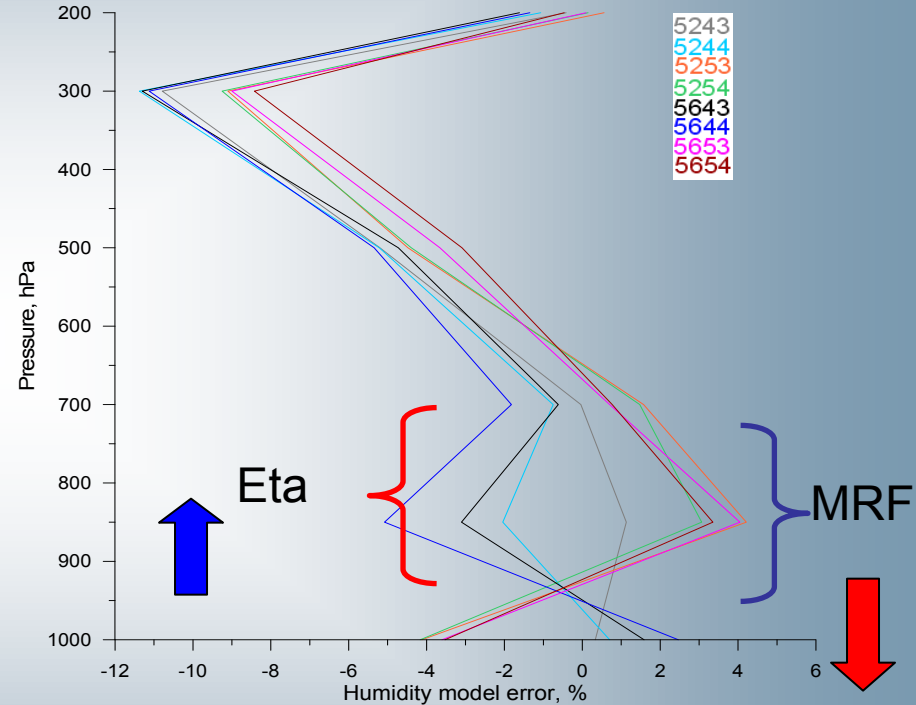
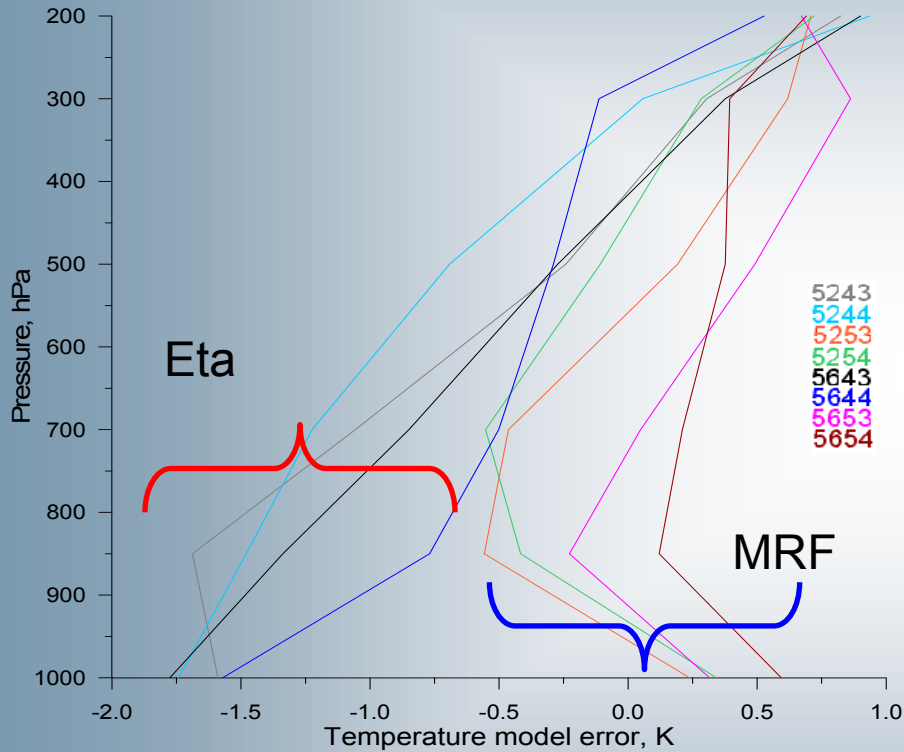
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# The sources of errors in NWP



\* A big challenge to separate a contribution from each source

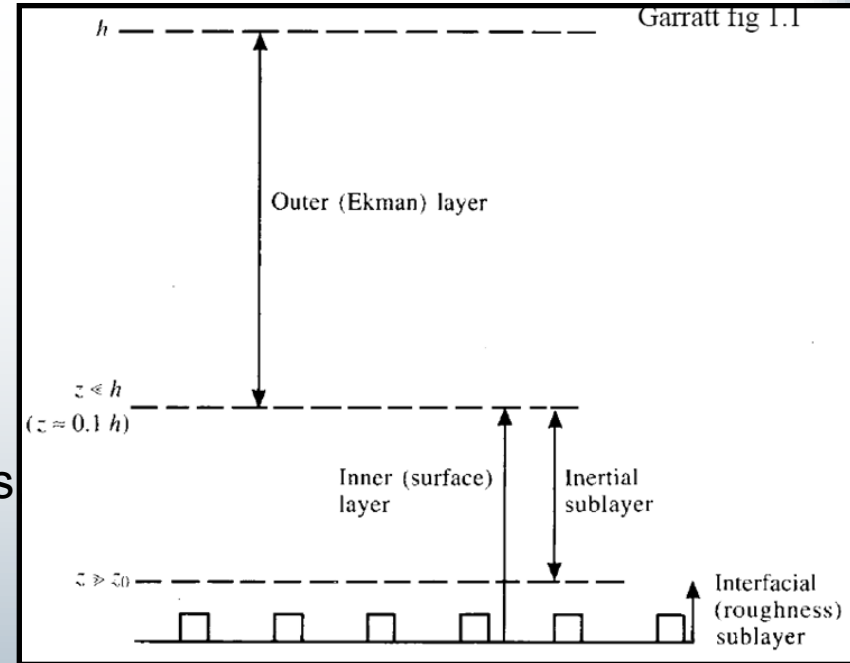
# Vertical profiles of the systematic error of temperature and relative humidity



Here compared model (MM5v3.7) fields against reanalysis ERA40 for the winter season of 2002 over the North Atlantic and Europe on a coarse resolution grid (81 km).

# Atmospheric (Planetary) Boundary Layer

- Large diurnal temperature variations
- Turbulence (owing to thermal forcing, vertical/horizontal wind shear)
- Gravity waves
- Spiraling Winds
- Katabatic (drainage) Winds
- Nocturnal Jet
- Clouds (Fair weather cumulus, trade cumulus stratocumulus clouds)
- Fog



## Kinds of ABL

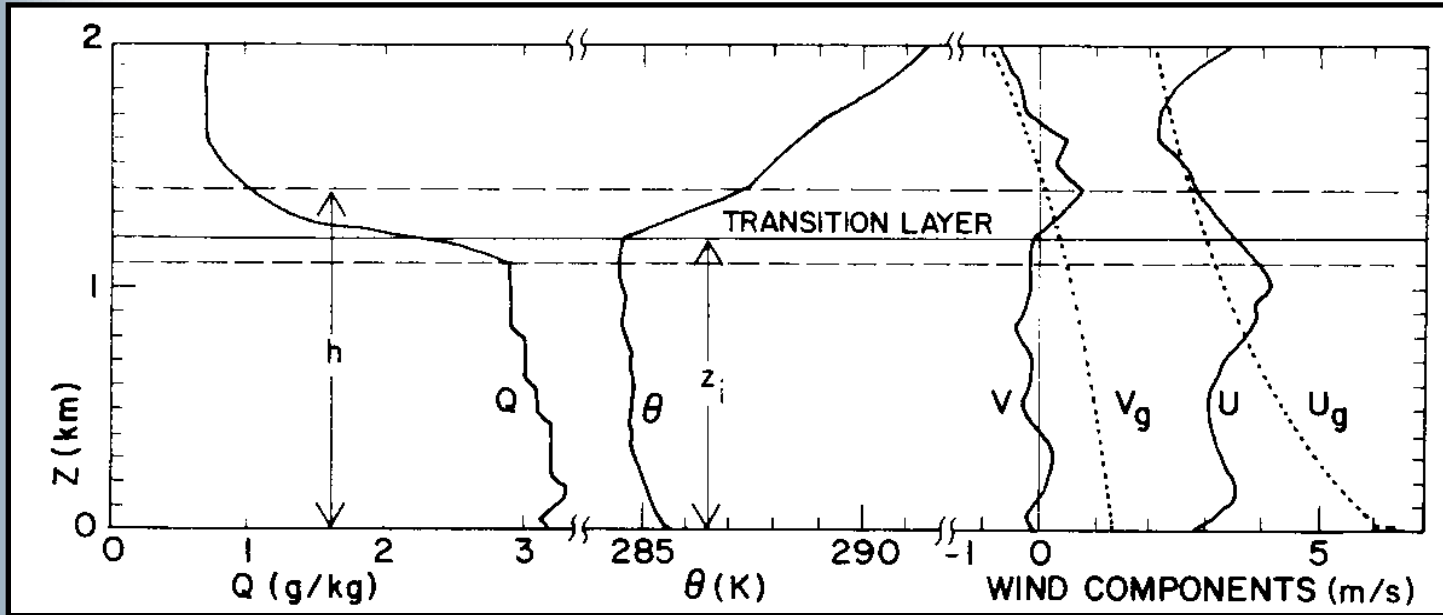
- Convective [  $Ri < 0$  ]
- Near-Neutral [  $Ri \approx 0$  ]
- Stable (very stable BL) [  $Ri \gg 1$  ]
- Marine/continental ABL*  
(according to surface properties)

## Zilitinkevich and Esau (2007)

- truly neutral (TN) ABL:  $F_* = 0, N = 0,$
  - conventionally neutral (CN) ABL:  
 $F_* = 0, N > 0,$
  - nocturnal stable (NS) ABL:  $F_* < 0, N = 0,$
  - long-lived stable (LS) ABL:  $F_* < 0, N > 0.$
- $F_*$  - potential temperature flux at the surface,  
 $N$  - Brunt-Väisälä frequency

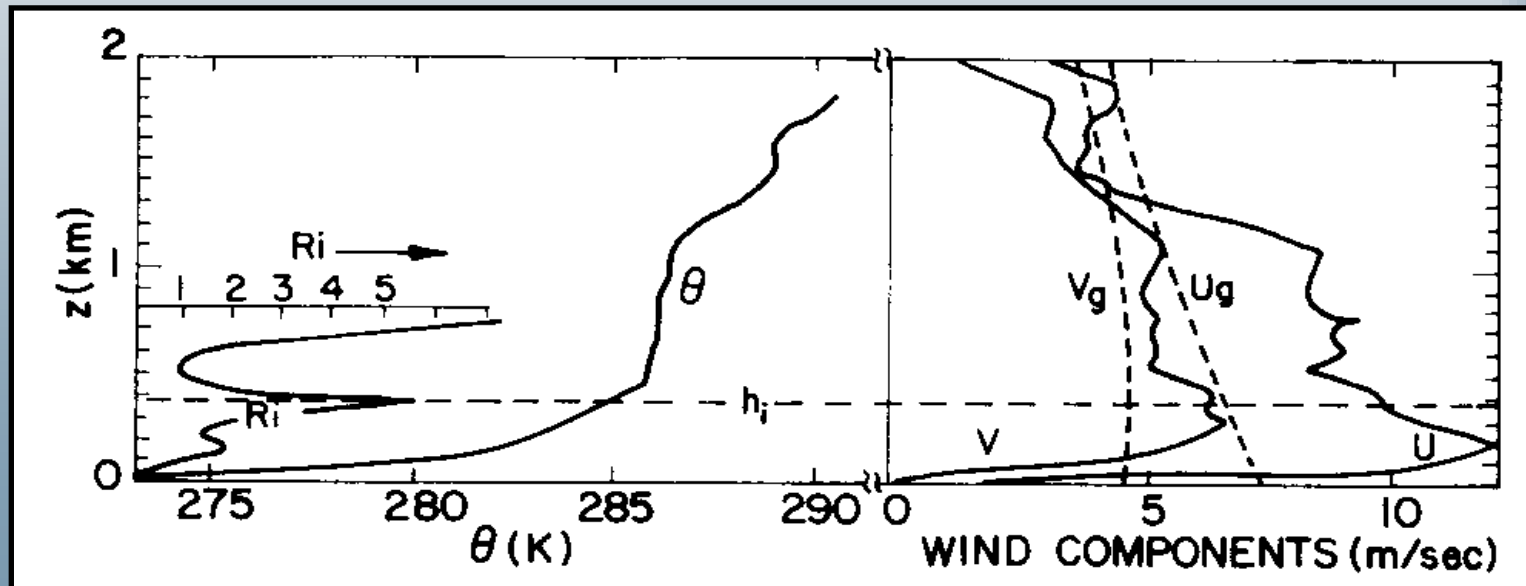
# Measured profiles in PBL under convective (a) and very stable (b) conditions

from Deardoff (1978)



a)

b)



WIND COMPONENTS (m/sec)

# Reynolds averaging

$$a = \bar{a} + a'$$

$a'$  fluctuating part or perturbation  
 $\bar{a}$  ensemble mean

$$\begin{aligned}\overline{\frac{Da}{Dt}} &= \overline{\frac{\partial a}{\partial t}} + \nabla \cdot \bar{\mathbf{u}}a \\ &= \frac{\partial}{\partial t}\bar{a} + \frac{\partial}{\partial t}\overline{a'} + \frac{\partial}{\partial x}\overline{(\bar{u} + u')(a + a')} + \frac{\partial}{\partial y}\overline{(\bar{v} + v')(a + a')} + \frac{\partial}{\partial z}\overline{(\bar{w} + w')(a + a')} \\ &= \frac{\partial}{\partial t}\bar{a} + \nabla \cdot \bar{\mathbf{u}}\bar{a} + \frac{\partial}{\partial x}\overline{u'a'} + \frac{\partial}{\partial y}\overline{v'a'} + \frac{\partial}{\partial z}\overline{w'a'}\end{aligned}$$



# General approaches in parameterization of ABL

## Mixed layer models

$$\overline{u}, \overline{v}, \overline{\theta} \rightarrow \text{uniform}$$

## 'Local' closures based on eddy diffusivity (K-theory)

$$\overline{w'a'} = -K_a \frac{d\overline{a}}{dz}$$

- **First-order closure**,  $K_a$  is specified from the vertical shear and static stability, or by prescribing  $\mathbf{a}$
- **1.5-order closure** or **TKE closure**, TKE is predicted with a prognostic energy equation, and  $K_a$  is specified using the TKE and some lengthscale.
- **K-profiles**, a specified profile of  $K_a$  is applied over a diagnosed turbulent layer depth.

## 'Nonlocal' closures

explicit model the effects of boundary layer filling eddies in some way.

*Horizontal turb. fluxes neglected*

# TKE budget equation

$$De/Dt = S + B + T + D$$

S = shear production;

B = bouyancy flux;

T = transport + pressure work;

D = dissipation

$$S = -\overline{u'w'}\frac{\partial\bar{u}}{\partial z} - \overline{v'w'}\frac{\partial\bar{v}}{\partial z}$$

$$B = \overline{w'b'}$$

$$T = -\frac{\partial}{\partial z}\left(\overline{w'e'} + \frac{1}{\rho_0}\overline{w'p'}\right)$$

$$D = -\nu\overline{|\nabla\times\mathbf{u}|^2}$$

## The flux Richardson number

$$Ri_f = -B/S$$

characterizes whether the flow is  
stable ( $Ri_f > 0$ ), neutral ( $Ri_f \approx 0$ ), or unstable ( $Ri_f < 0$ ).

# Problems in description of PBL

- PBL datasets (impacts of vertical advection, averaging time, stationarity, measurement height, site homogeneity, vertical alignment of the sensors, flow distortion).
- Spatial averaging of turbulent fluxes.
- In CABL cells and rolls in the shear free and sheared regimes, (respectively not well understood).
- Marine ABL constrained waters, coastal areas and lakes.
- Surface turbulent fluxes of momentum, heat and water vapour over the sea.
- The gas and particle exchange between the atmosphere and ocean
- Complex (sloping) surfaces
- Monin–Obukhov similarity theory unsatisfactory (over complex terrain, inadequately strongly stable and strongly unstable stratification regimes)

# General definition of $L_{MO}$ and $z_j$

$$L_{MO} = -\frac{\overline{\theta}}{gk} \cdot \frac{u_*^3}{\overline{w'\theta'}} \quad z_j = \frac{\pi}{4} \left( \frac{4K^2 \text{Pr}}{N^2 \sin^2(\alpha)} \right)^{1/4}$$

$$Ri = \frac{N^2}{(\partial U / \partial z)^2}$$

near-surface momentum flux

$$u_*^2 = K \text{Pr} \frac{\partial U}{\partial z}$$

heat flux

$$-\overline{w'\theta'} = K \frac{\partial \Theta}{\partial z}$$

$Pr$  – Prandtl number

$Ri$  – Richardson number

$g$  – gravity acceleration

$k$  – von Karman const.

$N$  – buoyancy frequency

$U$  – mean wind speed

$K$  – eddy heat conductivity

$\overline{w'\theta'}$  - near-surface heat flux

$u_*$  - friction velocity

$\overline{\theta}$  - relevant potential temperature

$\alpha$  - const. slope angle

1

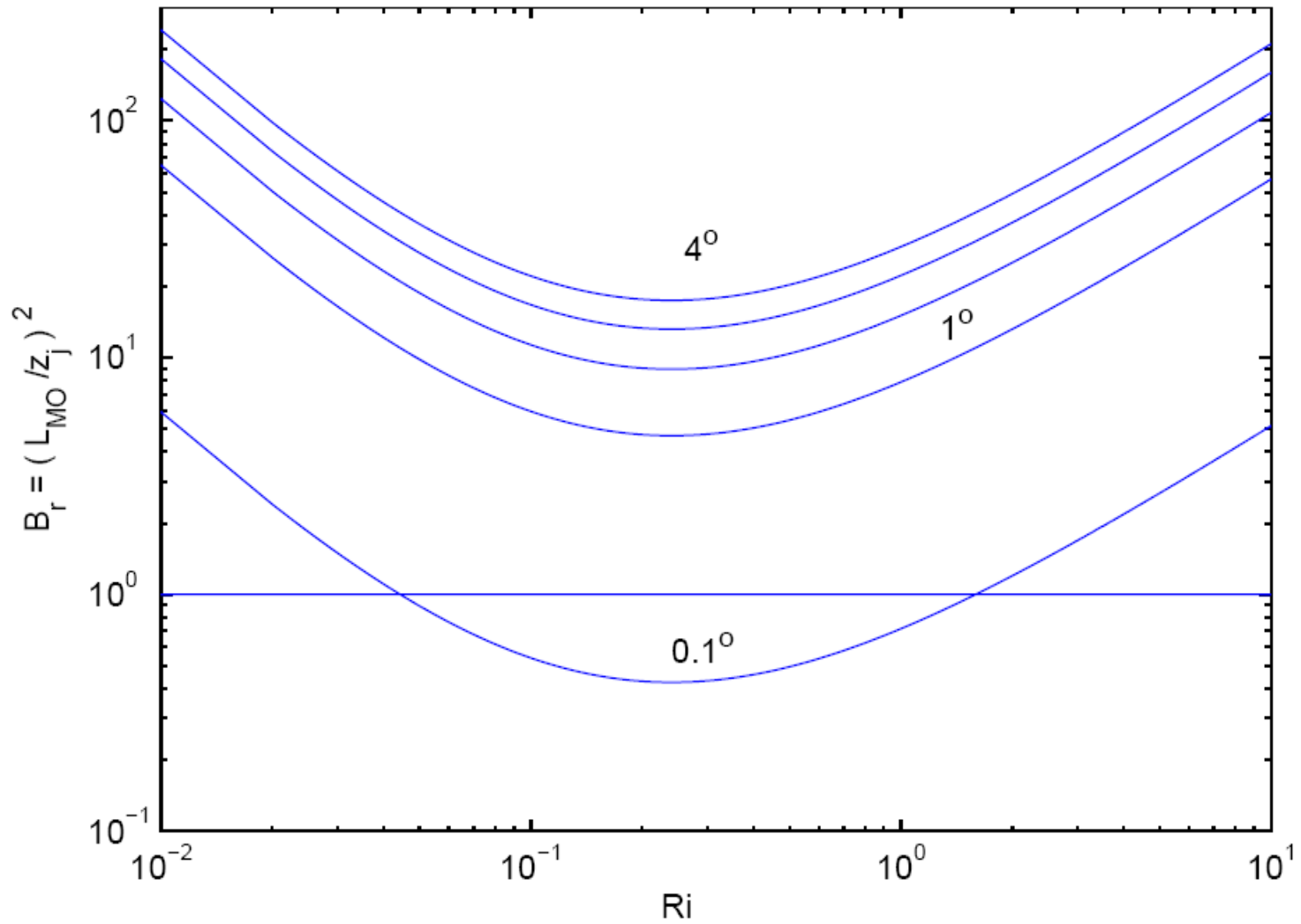
$$\left(\frac{L_{MO}}{z_j}\right)^2 = br = \frac{8}{(k\pi)^2} |\sin(\alpha)| \left(\frac{Pr^5}{Ri^3}\right)^{1/2}$$

$$Pr \approx 0.8 + 5 Ri$$

2

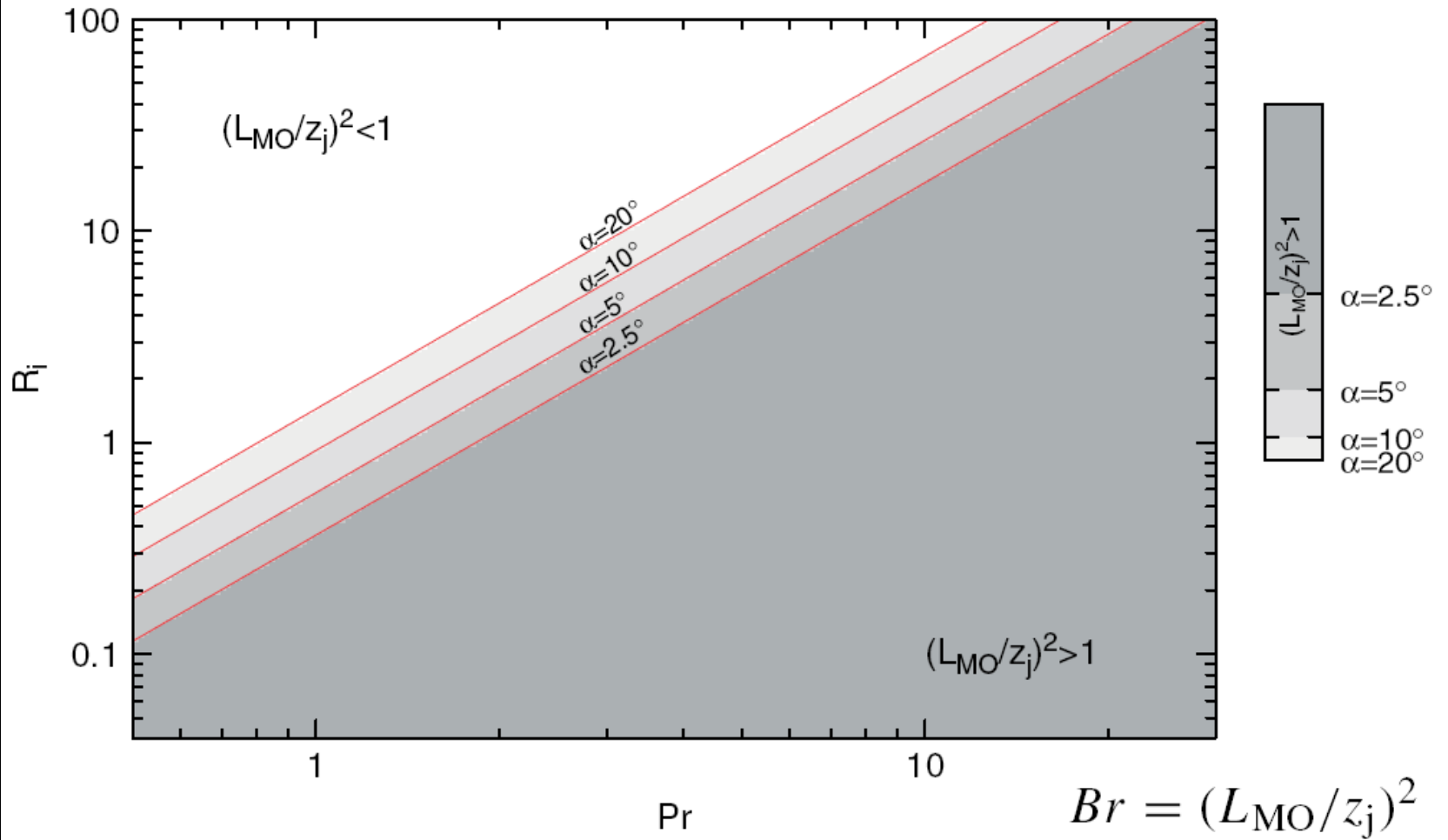
$$\left(\frac{L_{MO}}{z_j}\right)^2 = br = \frac{8}{(k\pi)^2} |\sin(\alpha)| \left(\frac{(0.8 + 5Ri)^5}{Ri^3}\right)^{1/2}$$

MONIN-OBUKHOV VS. LLJ HEIGHT OVER SMALL SLOPES



$k = 0.4, \quad L = L_{MO}$

# LOW-LEVEL KATABATIC JET HEIGHT



# Possible including $L_{MOD}$

3

$$L_{MOD} = \min(L, C_0 z_j)$$

4

$$\frac{1}{L_{MOD}} = \frac{c}{L} + \frac{d}{z_j}$$

$c, d$  should be obtained from measurements

$$0.7 < C_0 \leq 0.9$$



# Conclusions

The Monin-Obukhov scaling becomes inadequate to describe the lower part of sloped stably-stratified boundary layers dynamics.

For refining horizontal resolution in numerical models,  $L$  should accommodate slope effects on the near-surface turbulent fluxes.

It requires more testing and model comparisons using very high vertical resolution against various data sets.



Thanks

for your  
attention !

